

Chillicothe Road
Bainbridge Twp.
Sec. D.

DIETZGEN
TRADE MARK

ENGINEERS'
LEVEL BOOK
No. 410

171

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1 $\frac{1}{2}$ see inside of back cover.

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Chillicothe Road

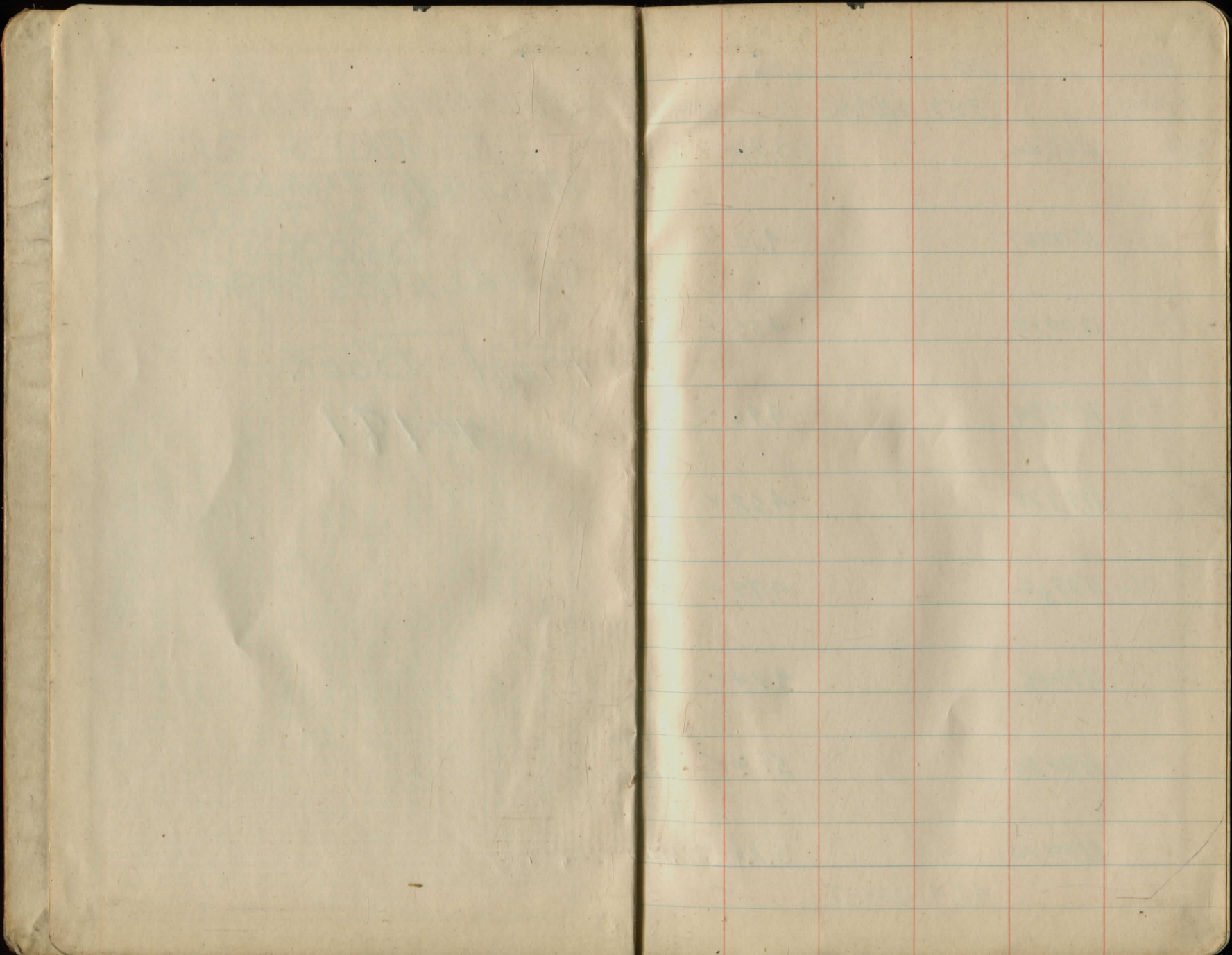
Sec D

Bainbridge Twp

Grade Stakes

Field Book

#171



Finished
Grade

7/10/28

Richey
WhiskinParks
Spohn

Sta

BS

HI

FS

TP259½

389

1209.40

1200.51

259

1200.44

3.96 ✓

+50 1200.27

4.13 ✓

258

1200.10

4.30 ✓

+50 1199.94

4.46 ✓

257

1199.78

4.62 ✓

+50 1199.62

4.78 ✓

256

1199.46

4.94 ✓

+50 1199.30

5.10 ✓

255

1199.14

5.26 ✓ 1199.14

4.24 1203.38

578

B3

H2

F5

120338

+50 1199.02

4.36 ✓

254 1198.96

4.42 ✓

+50 1198.96

4.42 ✓

253 1199.04

4.34 ✓

+50 1199.17

4.21 ✓

252 1199.39

3.99 ✓

+50 1199.66

3.72 ✓

251 1200.00

3.38 ✓

+50 1200.37

3.01 ✓

579

B5

H2

P5

120338

250

1200.75

2.63 ✓ 1200.75

6.15

1206.90

+50

1201.12

5.78 ✓

249

120150

5.40 ✓

+50

120187

5.03 ✓

New

BM #29

360

120686

360

1203.30

120326

248

1202.25

4.61 ✓

+50

120262

4.24 ✓

247

120300

3.86 ✓

+50

120337

3.49 ✓

246

120375

3.11 ✓

Sta BS HI FS

120686

+50 120412 2.74 ✓

245 120450 2.36 ✓ 120450

581 121031

+50 120487 5.44 ✓

244 120525 5.06 ✓

+50 120562 4.69 ✓

243 120600 4.31 ✓

+50 120637 3.94 ✓

242 120675 3.56 ✓

+50 120705 3.26 ✓

241 1207.22 400 1211.22 3.09 1207.22

sta BS HI FS

121122

+50 120724 3.98 ✓

240 120711 4.11 ✓

+50 120693 4.29 ✓

239 120674 4.48 ✓

+50 120656 4.66 ✓

238 120637 4.85 ✓

+50 120621 5.01 ✓

237 120610 4.63 121073 5.12 ✓ 120610

+50 120602 4.71 ✓

236 120600 4.73

Sta

BS

HI

PS

121673

750 120590

4.83

235

120580

B4 #28

3.14 1207.59

120759

7/20/95

Fisher
Park's
Whistler
Spokane

Sta	BS	HJ	FS
BM*5	0.98	1143.74	1142.76
42+00	1139.65		4.09
43+00	1136.22		7.52
44+00	1132.25		11.49
	0.40	1131.61	12.53
45+00	1128.00		3.61
46+00	1123.75		7.86
	0.78	1119.88	12.51
47+00	1119.50		0.38
48+00	1115.25		4.63
49+00	1111.00		8.88
	0.64	1107.43	13.09
50+00	1106.75		0.68

$$\frac{C2.1}{27.3} \quad \frac{C2.0}{26.3} \quad \frac{C1.7}{23.8} \quad \frac{C1.8}{26.8}$$

$$\frac{C2.4}{27.3} \quad \frac{C2.0}{27.3} \quad \frac{C1.8}{26.0} \quad \frac{C1.9}{27.0}$$

$$\frac{C2.2}{27.1} \quad \frac{C1.9}{26.1} \quad \frac{C1.3}{25.2} \quad \frac{C1.4}{26.2}$$

$$\frac{C1.1}{25.3} \quad \frac{C0.7}{24.2} \quad \frac{C1.6}{25.7} \quad \frac{C1.8}{26.7}$$

$$\frac{F3.1}{21.3} \quad \frac{F3.2}{20.3} \quad \frac{F2.9}{19.7} \quad \frac{F2.4}{20.7}$$

$$\frac{F4.6}{23.9} \quad \frac{F4.5}{22.9} \quad \frac{F6.1}{26.1} \quad \frac{F3.9}{27.1}$$

$$\frac{F1.1}{22.2} \quad \frac{F1.4}{21.2} \quad \frac{F2.7}{12.3} \quad \frac{F2.5}{20.3}$$

$$\frac{F1.2}{22.1} \quad \frac{F1.5}{21.1} \quad \frac{F1.9}{20.5} \quad \frac{F1.7}{21.5}$$

$$\frac{F1.1}{22.4} \quad \frac{F1.3}{21.4} \quad \frac{F2.0}{20.3} \quad \frac{F1.7}{21.3}$$

579

BS

HI

FS

1107.43

51+00 110250

4.93

52+00 109819

9.24

BM#6

5.62 1101.81 1101.83

53+00 109342

54+00 108814

55+00 108240

56+00 107660

57+00 107029

58+00 106669

59+00 106391

F1.2	F1.4
22.2	21.2

F1.7	F1.7
20.8	21.8

C2.6	C2.2
27.6	26.6

C0.1	C0.3
23.4	24.4

— 21.0

29.0 —

— 33.5

32.0 —

— 23.5

27.0 —

— 28.0

22.5 —

— 25.0

23.0 —

— 23.5

23.5 —

— 23.5

23.0 —

7/24/28

Richey Whiskin
Parks Spahn

Sta	B5	H2	F5
BAI#6	0.41	1102.24	1101.83
53+00			8.82
54+00			14.10
	1.80	1091.30	12.74 1089.50
55+00			8.90
	4.03	1082.77	12.56 1078.74
56+00			6.17
57+00			11.78
	2.42	1073.50	11.69 1071.58
58+00			6.81
59+00			9.59
60+00			11.07
	3.21	1064.44	12.27 1061.23
61+00			3.29

C7.1
34.7

C6.9
33.7

C3.9
29.0

C3.9
30.0

C7.8
35.4

C7.4
34.4

C4.7
30.3

C5.0
31.3

C6.0
33.1

C5.9
32.1

C2.6
27.2

C2.7
28.2

C2.5
28.0

C2.5
27.0

F0.3
22.9

C0.1
23.9

C0.1
24.0

F0.2
23.0

F0.6
22.4

F0.7
23.4

C0.8
25.9

C1.1
24.9

C0.2
23.6

C0.7
24.6

C0.1
24.3

C0.0
23.3

C0.0
23.3

C0.1
24.3

F1.2
22.5

F1.2
21.5

F1.4
21.2

F1.3
22.2

F1.1
22.5

F1.2
21.2

F2.0
20.3

F1.8
21.3

Sta BS HI FS

106444

62+00 1059.86 4.58

63+00 1058.57 5.87

64+00 1057.29 7.15

3.99 1060.88 8.35 1056.09

65+00 1056.32 3.76

66+00 1056.00 4.08

BM #7 5.63 1060.16 5.63 1054.45 1054.53

67+00 1056.00 4.16

68+00 1056.00 4.16

TP NW 1/4 Headwall 3.20 1056.96

69+00 1056.45

$\frac{F0.6}{23.3}$ $\frac{F0.7}{22.3}$ $\frac{F1.3}{20.5}$ $\frac{F1.4}{22.4}$

$\frac{F0.8}{23.1}$ $\frac{F0.9}{22.1}$ $\frac{F1.5}{21.2}$ $\frac{F1.5}{22.2}$

$\frac{F1.2}{22.8}$ $\frac{F1.0}{21.8}$ $\frac{F1.8}{20.6}$ $\frac{F1.8}{21.6}$

$\frac{F0.3}{23.7}$ $\frac{F0.4}{22.7}$ $\frac{F1.6}{20.9}$ $\frac{F1.5}{21.9}$

$\frac{F2.3}{20.7}$ $\frac{F2.4}{19.7}$ $\frac{F1.5}{22.1}$ $\frac{F1.7}{22.2}$

$\frac{F2.6}{20.3}$ $\frac{F2.7}{19.3}$ $\frac{F2.3}{19.9}$ $\frac{F2.3}{20.9}$

$\frac{F2.9}{20.7}$ $\frac{F2.9}{19.7}$ $\frac{F2.5}{19.6}$ $\frac{F2.3}{20.6}$

7/26/28

Kilney
Parks
Spencer
F5

STG	B5	H1	F5
72	12.31	1069.27	1056.96
69+00	1056.45	12.82	
70+00	1057.80	11.47	
71+00	1059.60	9.67	
72+00	1061.40	7.87	
73+00	1063.20	6.07	
	5.22	1071.14	3.35 1065.92
74+00	1065.00	6.14	
75+00	1066.80	4.34	
76+00	1068.60	2.54	
77+00	1070.40	0.74	
	12.06	1082.17	1.03 1070.11

F2.4 20.4	F2.6 19.4	F2.4 18.7	F2.6 20.7
--------------	--------------	--------------	--------------

F1.1 22.5	F1.2 21.5	F2.3 19.9	F2.1 20.9
--------------	--------------	--------------	--------------

C3.2 28.0	C2.5 27.0	C4.4 30.9	C4.6 30.9
--------------	--------------	--------------	--------------

C1.1 25.8	C1.0 24.8	C4.9 30.6	C5.1 31.6
--------------	--------------	--------------	--------------

C1.9 27.0	C1.8 26.0	C3.4 28.4	C3.6 27.4
--------------	--------------	--------------	--------------

C1.4 26.2	C1.3 25.2	C1.9 26.0	C2.2 27.1
--------------	--------------	--------------	--------------

C0.0 21.3	F2.0 20.3	F1.6 20.9	F1.0 21.2
--------------	--------------	--------------	--------------

F2.5 20.5	F2.8 19.5	F1.6 20.9	F1.1 21.9
--------------	--------------	--------------	--------------

F2.6 20.4	F2.6 19.4	F1.8 20.6	F1.6 21.6
--------------	--------------	--------------	--------------

Sta	BS	HI	FS
		1082.17	
78+00	1072.20		9.97
79+00	1074.00		8.17
80+00	1075.80		6.37
TP NEAR Headwall		1.00	1081.17
81+00	1077.60		
82+00	1079.40		
83+00	1081.20		
84+00	1083.11		
B.M. #9			
85+00			
86+00			

$\frac{F2.6}{21.0}$	$\frac{F30}{20.0}$	$\frac{F12}{21.5}$	$\frac{F1.1}{22.5}$
$\frac{F2.5}{21.7}$	$\frac{F34}{20.7}$	$\frac{C10}{24.8}$	$\frac{C1.1}{25.8}$
$\frac{C1.0}{23.5}$	$\frac{C08}{24.5}$	$\frac{C30}{27.8}$	$\frac{C3.2}{28.8}$
—	$\frac{24.0}{}$	$\frac{27.0}{}$	—
—	$\frac{22.5}{}$	$\frac{24.0}{}$	—
—	$\frac{21.0}{}$	$\frac{22.5}{}$	—
—	$\frac{20.0}{}$	$\frac{22.5}{}$	—
1085.05	—	—	—
—	$\frac{20.0}{}$	$\frac{20.0}{}$	—
—	$\frac{21.0}{}$	$\frac{20.5}{}$	—

7/27/25

NICHOL
SPARKS
SPANN

Sta

BS

HI

FS

TP

3.97 1085.14

1081.17

81+00 1077.60

7.54

 $\frac{C0.6}{24.6}$ $\frac{C0.2}{23.6}$ $\frac{C2.6}{27.2}$ $\frac{C2.7}{28.2}$

82+00 1079.40

5.74

 $\frac{F0.4}{23.3}$ $\frac{F0.7}{22.3}$ $\frac{C1.2}{25.1}$ $\frac{C1.4}{26.1}$

83+00 1081.20

3.94 ✓

 $\frac{F1.9}{21.2}$ $\frac{F2.1}{20.2}$ $\frac{C0.2}{23.6}$ $\frac{C0.1}{24.6}$

84+00 1083.11

2.03 ✓

 $\frac{F3.0}{21.1}$ $\frac{F3.1}{20.1}$ $\frac{F1.1}{21.7}$ $\frac{F0.7}{22.7}$

8.99 1092.70 1.23 1083.91

85+00 1085.24

7.46 ✓

 $\frac{F3.7}{22.5}$ $\frac{F3.8}{21.5}$ $\frac{F2.5}{20.5}$ $\frac{F2.4}{20.6}$

BM # 9

7.56 1092.61 7.56 1085.14 1085.05

86+00 1087.49

5.12

 $\frac{F3.0}{21.5}$ $\frac{F3.3}{20.5}$ $\frac{F3.3}{20.5}$ $\frac{F3.0}{21.5}$

87+00 1089.75

2.86

 $\frac{F1.6}{21.6}$ $\frac{F1.8}{20.6}$ $\frac{F0.4}{22.7}$ $\frac{C0.0}{23.7}$

8.73 1101.33 0.01 1092.60

88+00 1092.00

9.33

 $\frac{F1.2}{22.2}$ $\frac{F1.4}{21.3}$ $\frac{C0.1}{23.4}$ $\frac{C0.4}{24.4}$

89+00 1094.24

7.09

 $\frac{C0.1}{24.3}$ $\frac{C0.0}{23.3}$ $\frac{C3.8}{29.0}$ $\frac{C4.1}{30.0}$

Sta	BS	HI	FS
		1101.33	
90+00	1096.48		4.85
		940	1110.45
91+00	1098.72		11.73
92+00	1100.96		9.49
93+00	1103.20		7.25
TP		967	1110.10
94+00	1105.44		4.56
95+00	1107.68		2.42
		12.05	1118.99
BM #10		862	1118.89
96+00	1109.92		8.97
97+00	1112.16		
98+00	1114.32		

$\frac{C08}{25.2}$	$\frac{C06}{24.2}$	$\frac{C30}{27.8}$	$\frac{C31}{28.8}$
$\frac{C22}{27.3}$	$\frac{C20}{26.3}$	$\frac{C47}{30.3}$	$\frac{C49}{31.3}$
$\frac{C22}{27.6}$	$\frac{C22}{26.6}$	$\frac{C57}{31.8}$	$\frac{C56}{32.8}$
$\frac{C09}{25.6}$	$\frac{C09}{24.6}$	$\frac{C42}{22.6}$	$\frac{C43}{30.6}$
$\frac{F82}{30.5}$	$\frac{F78}{29.5}$	$\frac{F63}{26.5}$	$\frac{F62}{27.5}$
	1110.27		
$\frac{F48}{25.3}$	$\frac{F52}{24.3}$	$\frac{F67}{27.3}$	$\frac{F67}{28.3}$
$\frac{F28}{20.7}$	$\frac{F29}{19.7}$	$\frac{C09}{24.6}$	$\frac{C1.2}{25.6}$
—	$\frac{22}{22}$	$\frac{28}{28}$	
—	$\frac{25}{25}$	$\frac{33}{33}$	

8/3/28

Richey
Parks
Spahn

Sta	BS	HJ	FS	
BM #10	12.27	1122.54		1110.27
97+00	1112.16		10.38	
98+00	1114.32		8.22	
99+00	1116.58		5.96	
	5.30	1121.12	6.72	1115.82
100+00	1118.82		2.30	
	13.06	1128.88	5.30	1115.82
101+00	1120.06		8.82	
102+00	1123.32		5.56	
BM #11	7.43	1129.53	6.90	1121.98
103+00	1125.69		3.94	1122.10
104+00	1127.87		1.66	
	10.37	1139.76	0.14	1129.39
105+00	1130.30		2.46	

$\frac{C1.1}{26.1}$	$\frac{C1.2}{25.1}$	$\frac{C3.7}{28.8}$	$\frac{C4.0}{29.8}$
$\frac{C2.2}{26.4}$	$\frac{C1.4}{25.4}$	$\frac{C6.6}{33.2}$	$\frac{C6.7}{34.2}$
$\frac{C0.4}{25.0}$	$\frac{C0.5}{24.0}$	$\frac{C6.2}{32.6}$	$\frac{C6.5}{33.6}$
$\frac{F10.5}{35.9}$	$\frac{F10.0}{34.9}$	7' Berm $\frac{F1.5}{22.1}$	$\frac{F1.2}{23.1}$
$\frac{F3.1}{22.5}$	$\frac{F3.3}{21.5}$	7' Berm $\frac{F1.5}{22.1}$	$\frac{F1.3}{23.1}$
$\frac{C1.6}{26.4}$	$\frac{C1.4}{25.4}$	$\frac{C5.4}{31.4}$	$\frac{C5.8}{32.4}$
$\frac{F4.2}{23.1}$	$\frac{F4.1}{22.1}$	7' Berms $\frac{F8.0}{30.6}$	$\frac{F8.1}{31.6}$
$\frac{F2.8}{21.3}$	$\frac{F3.2}{20.3}$	$\frac{F2.8}{19.5}$	$\frac{F3.1}{20.5}$
$\frac{C0.1}{23.7}$	$\frac{E0.4}{22.7}$	$\frac{F1.3}{21.4}$	$\frac{F0.1}{22.4}$

579

B5

HI

F5

1139.76

106+00 1133.87

5.89

11.71 1151.29 0.18 1139.58

107+00 1138.61

12.68

108+00 1143.52

7.77

TP slope L

2.97 1148.32

109+00 1148.43

110+00 1153.34

111+00 1158.25

112+00 1163.05

113+00 1166.86

114+00 1169.04

BM #12

 $\frac{F0.9}{22.4}$ $\frac{F1.3}{21.4}$ $\frac{F1.8}{20.6}$ $\frac{F1.7}{21.6}$ $\frac{C5.0}{31.3}$ $\frac{C4.7}{30.3}$ $\frac{C1.5}{25.5}$ $\frac{C1.2}{26.5}$ $\frac{C4.8}{31.3}$ $\frac{C4.7}{30.3}$ $\frac{C4.6}{30.2}$ $\frac{C4.2}{31.2}$

— 27

27

— 26

23

— 20

25

— 26

25

— 24

23

— 24

21

8/9/28

Sta	B5	HI	F5
TP	12.79	1161.11	1148.32
109+00	1148.43		12.68
110+00	1153.34		7.77
111+00	1158.25		2.86
	11.96	1171.82	125 1159.86
112+00	1163.05		8.77
113+00	1166.86		4.96
114+00	1169.04		2.78
BM #12			2.05 1169.77 1169.75
115+00	1170.35		

$\frac{C32}{28.8}$	$\frac{C30}{27.8}$	$\frac{C17}{25.8}$	$\frac{C1.7}{26.8}$
$\frac{C20}{27.1}$	$\frac{C19}{26.1}$	$\frac{C04}{23.9}$	$\frac{C0.6}{24.9}$
$\frac{C1.6}{26.2}$	$\frac{C1.3}{25.2}$	$\frac{C1.2}{25.1}$	$\frac{C1.6}{26.1}$
$\frac{C1.7}{26.4}$	$\frac{C1.4}{25.4}$	$\frac{C17}{25.8}$	$\frac{C2.1}{26.8}$
$\frac{C1.4}{25.9}$	$\frac{C1.1}{24.9}$	$\frac{F02}{23.0}$	$\frac{C0.0}{24.0}$
$\frac{C0.7}{25.0}$	$\frac{C0.5}{24.0}$	$\frac{F07}{22.3}$	$\frac{F0.6}{23.3}$

Grade Changed

8/14/23

Richey
Parks
5pohn

Sta

BS

HI

FS

BM #24	0.85	1164.91		1164.06
	0.60	1152.50	13.01	1151.90
	0.60	1140.50	12.60	1139.98
	0.20	1127.61	13.09	1127.41
	0.63	1115.41	12.83	1114.78

203+00 1166.61 8.80

F4.6
24.3

F4.7
23.3

 7' Berm

F3.4
21.7

F3.2
22.7

204+00 1115.13 0.28

F0.2
24.4

F0.6
23.4

 7' Berm

F4.1
23.1

F4.5
24.1

12.58 1127.51 0.98 1114.93

205+00 1123.85 3.66

F0.7
23.8

F1.0
22.7

 7' Berm

F2.1
21.2

F2.1
22.2

13.00 1140.39 0.12 1127.39

206+00 1132.57 7.82 F9

C2.7
28.0

C2.5
27.0

C1.2
25.7

C1.5
26.1

13.10 1152.88 0.51 1139.88

207+00 1141.27 11.61 C1

C2.6
27.4

C2.1
26.4

C5.3
31.2

C5.3
32.2

208+00 1149.77 3.11 F0.3

C1.2
25.0

C0.5
24.0

C1.0
24.8

C1.2
25.8

12.98 1164.86 1.00 1151.88

BM #24 0.82 1164.04

116486

209+00 1158.27

6.59 c.2

$\frac{C14}{265}$

$\frac{C15}{255}$

$\frac{C11}{249}$

$\frac{C13}{259}$

BM# 24

1199

117605

116406

210+00 1166.87

9.18

$\frac{C09}{25.2}$

$\frac{C06}{24.2}$

$\frac{C08}{24.6}$

$\frac{C10}{25.6}$

1165

1187.42

0.28

1175.77

211+00 1175.47

11.95

$\frac{C23}{27.1}$

$\frac{C19}{26.1}$

$\frac{C16}{25.7}$

$\frac{C18}{26.7}$

212+00 1183.82

3.60

$\frac{C18}{27.3}$

$\frac{C20}{26.3}$

$\frac{C02}{23.6}$

$\frac{C03}{24.6}$

Sta	B s	HT	G Rod	Ele. 1169.75
	446	1174.21		
115+00	1170.35		386	
116+00	1170.03		4.18	
117+00	1168.69		5.52	
118+00	1167.26		6.95	
119+00	1165.83		8.38	
	338	1166.94	10.65	1163.56
120+00	1164.43		251	
121+00	1163.36		358	
BM 154			3.10	1163.84
122+00	1163.00		3.94	

1163.84
 1163.84
 23-3

F0.6 23.1	F0.8 22.1	F1.8 20.6	F1.6 21.6
F0.6 22.4	F1.2 21.4	F1.1 21.7	F0.7 22.7
F0.1 24.1	F0.1 23.1	G0.5 24.2	G0.7 25.2
F0.5 23.4	F0.5 22.4	G0.7 24.4	G0.7 25.4
F1.7 21.6	F1.8 20.6	F0.8 22.1	F0.8 23.1
EL.6 21.7	F1.7 20.7	F0.5 22.4	F0.7 23.4
F1.4 21.7	F1.7 20.7	F0.6 22.2	F0.7 23.2
1163.84 F1.9 21.3	F2.0 20.3	F1.3 21.2	F1.3 22.2

Sta. B.S. H.I. Rod Elev

25-30

123+00 1163.00 394

124+00 1163.00 394
649 1160.45
6.26 1166.71

125+00 1163.00 371

126+00 1163.17 354
238 1164.33
4.37 1168.70

127+00 1163.94 536

128+00 1163.50 520
225 398 1168.77 398 1164.72

129+00 1163.67 510

130+00 1163.83 494

F3.0 F3.1 F2.9 F2.5
19.7 18.7 19.7 20.7

F3.0 F2.7 F1.7 F1.6
20.9 19.9 20.8 21.8

F1.6 F1.8 F0.2 F0.3
21.6 20.6 23.0 24.0

F0.4 F0.5 C0.9 C1.0
23.4 22.4 24.7 25.7

C0.4 C0.3 C1.9 C2.0
24.8 23.8 26.2 27.2

C1.0 C0.8 C2.3 C2.1
25.5 24.5 26.8 27.8

BM # 14 1164.79

C0.0 F0.1 C1.8 C1.6
24.1 23.1 25.2 26.2

F1.0 F1.1 C0.2 C0.3
22.7 21.7 23.6 24.6

Sta

B.S.

H.I.

F.S.

Elev

131100 1163.04

5.73

543 1163.34 T.P.

23-3

G03
24.6

G02

23.6

G11

24.9

G13
25.9

Finished Grade
Sta Grade HI FS

8/18/28

Richey
Whistler
Parks
Spohn

1203.61

213+50	1192.77		10.84	-
214	1194.82		8.79	-
+50	1196.37		7.24	-
215	1197.66		5.95	-
+50	1198.95		4.66	-
216	1200.24		3.37	-
+50	1201.53		2.08	-
217	1202.82		0.79	-
+50	1204.11	1211.85	7.74	-
218	1205.40		6.45	-
+50	1206.58		5.27	-
219	1207.52		4.33	-
+50	1208.21		3.64	-
220	1208.67		3.18	-
+50	1209.00		2.85	-
221	1209.33		2.52	-
+50	1209.67		2.18	-
222	1210.00	1215.36	5.36	-

1199.48

4.13

1203.61

0.79

1202.82

9.03

1211.85

2.18

1209.67

5.69

1215.36

121536

	+50	1210.33		5.03	-
223		1210.67		4.69	-
	+50	1211.00		4.36	-
224		1211.33	1215.39	4.06	-
	+50	1211.61		3.78	✓
225		1211.98		3.61	✓
	+50	1211.84		3.55	✓
226		1211.80		3.59	✓
	+50	1211.70		3.69	✓
227		1211.60	1215.32	3.72	-
	+50	1211.50		3.82	-
228		1211.40		3.92	✓
	+50	1211.30		4.02	✓
229		1211.20		4.12	-
	+50	1211.01		4.31	-
230		1210.63	1215.31	4.68	-
	+50	1210.08		5.23	-
231		1209.34		5.97	-

121536

B.M.		921		
		1211.15		
		1211.18		
		421		
		1215.39		
		370		
		1211.69		
		363		
		1215.32		
		273		
B.M.		1212.59		
B.M.		1212.58		
		2.73		
		1215.31		
		5.97		
		1209.34		

1211.89

+50 1208.50

3.39 -

232 1207.67

4.22 -

+50 1206.94

4.95 -

233 1206.42

5.47 -

+50 1206.11

5.78

234 1206.00

5.89

+50 1206.00

1209.34

2.55

1211.89

BM

1207.59

8/24/28
Kroner
Whiskey
Parks
Spain

Sta	BS	HI	FS	
BM #15	9060	1164.45		1153.85
132+00	1160.34		4.11	
133+00	1156.92		7.53	
134+00	1155.25		9.20	
BM #15	6.65	1160.50		1153.85
135+00	1155.92		4.58	
136+00	1158.33		2.17	
	12.29	1167.02	5.77	1154.73
137+00	1161.00		6.02	
138+00	1163.67		3.35	
	9.58	1173.85	2.75	1164.27
139+00	1166.33		7.52	
140+00	1168.24		5.61	

$\frac{C1.1}{25.8}$	$\frac{C1.0}{24.8}$	$\frac{C0.3}{23.7}$	$\frac{C0.7}{24.7}$
$\frac{C0.8}{22.0}$	$\frac{C0.5}{24.0}$	$\frac{C3.5}{28.5}$	$\frac{C3.9}{29.5}$
$\frac{F2.1}{20.9}$	$\frac{F2.3}{19.9}$	$\frac{F1.8}{20.6}$	$\frac{F1.5}{21.6}$
$\frac{F3.5}{21.7}$	$\frac{F3.4}{20.7}$	$\frac{F4.3}{22.5}$	$\frac{F4.2}{23.5}$
$\frac{F3.6}{22.3}$	$\frac{F3.7}{21.3}$	$\frac{F2.5}{19.6}$	$\frac{F1.9}{20.6}$
$\frac{F2.4}{20.3}$	$\frac{F2.7}{19.3}$	$\frac{F0.5}{22.6}$	$\frac{F0.2}{23.6}$
$\frac{C0.6}{24.9}$	$\frac{C0.4}{23.9}$	$\frac{C2.4}{26.9}$	$\frac{C2.5}{27.9}$
$\frac{C1.2}{25.6}$	$\frac{C0.9}{24.6}$	$\frac{C3.7}{28.8}$	$\frac{C3.9}{29.8}$
$\frac{\$ Road}{24.0}$		$\frac{C1.3}{25.2}$	$\frac{C1.5}{26.2}$

Sta	BS	HI	FS
141+00	1168.62		5.23
142+00	1168.24	287 1171.30 1170.39	542 7168.43 306
143+00	1167.88		342
144+00	1167.50		380
145+00	1167.13		417
BM #145+00			7.67 1163.63
146+10	1166.75		2.07 1169.22
147+00	1166.48		
148+00	1166.25		
149+00	1168.27		
150+00	1170.32		

F0.5 23.1	F06 23.1	F04 22.7	F01 23.7
F2.6 20.5	F26 19.5	F17 20.9	F14 21.9
F27 20.7	F29 19.7	F24 19.7	F22 20.7
F28 21.1	F31 20.1	F20 20.3	F17 21.3
F35 22.9	F40 21.9	F08 22.5	F03 23.5
—	200	230	—
—	225	200	—
—	230	200	—
—	260	260	—
—	25	26	—

1169.31

8/27/28 Richey Parks
Whiskin Spahn

Sta	BS	HI	FS
B4 145+00	192	117123	1169.31
147+00			4.75
148+00			4.28
149+00			2.96
	10.18	1179.67	1.74 1169.49
150+00			9.35
151+00			7.19
152+00			5.03
153+00			2.87
	8.16	1186.54	1.29 1178.38
154+00			7.58
155+00			5.42

F24
20.3

F27
19.3

F22
20.0

F2.3
21.0

F0.8
22.8

F1.0
21.8

F1.7
20.8

F1.6
21.8

C2.6
26.4

C14
25.4

C21
26.4

C2.1
27.4

C1.7
26.5

C1.5
25.5

C2.3
26.7

C2.5
27.7

C0.9
25.6

C0.9
24.6

C1.7
25.8

C1.7
26.8

F0.1
24.0

F0.2
23.0

C0.7
24.3

C0.9
25.3

F1.5
21.2

F21
20.2

C0.4
23.9

C0.3
24.9

F2.3
21.0

F22
20.0

C0.5
24.0

C0.7
25.0

F1.6
20.7

F2.9
19.7

C0.4
23.9

C0.6
24.9

Sta	BS	HI	FS
156+00	1183.28	1186.54	3.26
	1104	1195.09	249 1184.05
157+00	1185.44		9.55
158+00	1187.60		7.49
BM # 16			4.21 1190.88
159+00	1189.76		

F0.9 224	F13 214	F02 230	C02 240
F0.9 21.9	F.16 20.9	C05 290	C06 25.0
C1.5 26.5	C1.5 25.5	C1.5 25.5	C1.4 26.5

160

Finished Grade

8/27/28

grade HI F5

BM #23

1071.40

1063.32

196 1063.98 7.42 ✓

+50 1064.04 7.36 ✓

197 1064.44 6.96 ✓

+50 1065.53 5.87 ✓

198 1067.32 4.08 ✓

+50 1069.80 1.60 ✓

199 1072.98 1081.01 8.03 ✓

+50 1076.84 4.17 ✓

200 1081.05 1088.90 7.85 ✓

+50 1085.26 3.64 ✓

201 1089.47 1096.37 6.90 ✓

+50 1093.68 2.69 ✓

202 1097.89

+50 1102.10

1063.32

8.08

1071.40

1.61

1069.79

11.22

1081.01

4.17

1076.84

12.06

1088.90

3.66

1085.24

11.13

1096.37

1096.37

3.49

349

1092.88

89.47

3.41

1171.40

69.80

1.60

1081.01

72.98

8.03

1081.01

76.84

4.17

1088.90

81.05

7.85

1088.90

15.26

3.64

1096.37

89.47

6.90

1096.37

3.68

2.69

8/28/28

STA BS MJ FS

BM #22 105309

1064.92

191+00 1061.00 3.92 ✓

+50 1061.93 2.99 ✓

192 1062.65 2.33 ✓

+50 1063.19 1.83 ✓

193 1063.53 1.39 ✓

+50 1063.68 1.24 ✓

194 1063.74 1067.89 4.15 ✓

+50 1063.80 4.09 ✓

195 1063.86 4.03 ✓

+50 1063.92 3.97 ✓

196 1063.98 3.91

+50 1064.04 3.85

197 1064.44 3.45

BM #23 106332

105309
 11.83
 1064.92
 124
 106368
 421
 106789

Sta #	Grade	H.T.	F.S.	Elev.
BM 25		1200.22		1199.48
+50	1192.77		7.45 ✓	
213	1190.20		10.02 ✓	
+50	1187.32		12.90 ✓	
212	1183.92	1188.51	4.59 -	
+50	1180.02		8.49 -	
211	1175.87		12.64 ✓	
+50	1171.52	1177.22	5.70 -	
210	1167.12		10.10 -	
+50	1162.82	1165.32	2.50 -	
209	1158.47		6.85 ✓	
+50	1154.12	1164.20	10.08 ✓	
208	1149.77	1155.14	5.37 ✓	
+50	1145.52		9.62 ✓	
207	1141.27	1144.17	2.90 ✓	
+50	1136.82		7.35 ✓	
206	1132.47		11.70 ✓	
+50	1128.06	1133.20	5.14 ✓	
205	1123.85		9.35 ✓	

Date
8-29-28

0.74	575	1200.22
1199.48	1200.22	1200.22
0.74	92.77	91.20
1200.22	7.45	10.02
12.90		1164.20
1187.32		58.47
1.19		5.73
1188.51	1164.66	
12.94	13.16	
1175.57	1177.22	
1.65	1.35	
1177.22	1175.87	
13.16	12.60	
BM #24 1164.06	1188.47	
1.26		
1165.32		

7722	BM #24	1164.20
75.87	1164.06	54.12
1.35	0.14	10.08
88.47	1164.20	
8.002	14.06	
8.45	1154.14	
	1.00	
	1155.14	
	12.80	
	1142.34	
	1.83	
	1144.17	
	11.70	
	1132.47	
	0.73	
	1133.20	

Sta. Grade H.T. F.S.

+50	1119.44	1124.38	4.94 ✓
204	1115.13		9.25 ✓
+50	1110.92	1116.39	5.47 ✓
203	1106.61		9.78 ✓
+50	1102.20	1107.04	4.84 ✓
202	1097.89		9.15 ✓
+50	1093.68		13.36 ✓

chk. 01

1337

1124.38
 19.44
 494

1280
 57
 1337

1133.20

9.35

1123.85

0.53

1124.38

9.25

1115.13

1.26

1116.39

9.78

1106.61

0.43

1107.04

1093.68

13.36

1107.04

1097.89

9.15

1107.04

1093.68

13.36

5/3/28 Richey Parks
Whistler Spahn

Sta	Grade	H.I.	
		1200.84	
+50	1187.22		
213	1190.00	10.84	-
+50	1192.57	8.27	-
214	1194.62	6.22	-
+50	1196.17	4.67	-
215	1197.46	3.38	-
+50	1198.75	2.09	-
216	1200.04	0.80	-
+50	1201.33	1209.10	7.77 -
217	1202.62	6.48	-
+50	1203.91	5.19	-
218	1205.20	3.90	-
+50	1206.43	2.67	
219	1207.42	1.68	-
+50	1208.11	0.99	-
220	1208.57	0.53	-
+50	1208.90	1214.70	5.80 -
221	1209.23	5.47	-

BM #25

1199.48
1.36
1200.84
0.80
1200.04
9.06
1209.10
0.53
1208.57
6.13
1214.70

Sta	Grade	HI	
+50	1209.57	121470	5.13 ✓
222	1209.90		4.80 ✓
+50	1210.23		4.47 ✓
223	1210.57		4.13 ✓
+50	1210.90		3.80 ✓
224	1211.23	1216.10	4.87 ✓
+50	1211.46		4.64 ✓
225	1211.58		4.52 ✓
+50	1211.64		4.46 ✓
226	1211.60		4.50 ✓
+50	1211.50		4.60 ✓
227	1211.40		4.70 ✓
+50	1211.35		4.75 ✓
228	1211.30		4.80 ✓
+50	1211.25		4.85 ✓
229	1211.20	OK	4.90 ✓
+50			
230			

1214.70
 353
 1211.17
 1211.18
 492
 1216.10
 BM #26 1211.18
 BM #27 1212.58

Revised Grade ^{8/31/28}

Sta	BS	HI	FS
BM #	10.79	106388	105309
190+00	1058.74		5.19
189+00	1055.36		8.52
BM #	2.98	105754	105456
187+00	1052.63		4.91
186+00	1057.21		0.33
185+50	1061.02		-3.48

$\frac{C0.7}{17.0}$	$\frac{F0.6}{16.2}$	Special	$\frac{21.8}{22.5}$	$\frac{C1.5}{23.5}$
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$\frac{C3.5}{18.5}$	$\frac{C2.3}{17.5}$	Special	$\frac{C1.1}{22.4}$	$\frac{C0.9}{23.4}$
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$\frac{F5.8}{31.6}$	$\frac{F5.3}{30.6}$		$\frac{F5.3}{26.6}$	$\frac{F4.5}{27.6}$
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$\frac{F9.3}{39.0}$	$\frac{F7.0}{38.0}$		$\frac{F7.0}{30.0}$	$\frac{F6.1}{31.0}$
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$\frac{F6.4}{39.6}$	$\frac{F5.9}{32.6}$		$\frac{F9.4}{34.8}$	$\frac{F8.7}{35.8}$
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Finished Grade

BM #2

Whiskiri.
Snyder
Spotin

9/18/28

Sta	B.S.	H.I.	F.S.	1075.48
	0.02	1075.50		
			8.48	1067.02
	1.14	1068.16		
6+50	1060.02		8.14	✓
7+00	1061.60		6.56	✓
+50	1063.26		4.90	✓
8+00	1064.97		3.19	✓
+50	1066.68		1.29	1066.88 ✓
	9.55	1076.43		
9+00	1068.39		8.04	✓
+50	1070.10		6.33	✓
10+00	1071.81		4.62	✓
BM #2			0.93	1075.50

T.P

T.P

BM #2

1075.48

1075.48	1076.43
.02	93
1075.50	1075.50
8.48	
1067.02	
1.14	
1068.16	
1.28	
1066.88	
9.55	
1076.43	

Sta.	B.S.	H.I.	I.S.	BM #2
	0.93	1076.41		1075.48
+50	1075.52		2.89	✓
11100	1075.23		1.18	1075.23 ✓
	12.27	1087.50		
+50	1076.94		10.56	✓
12100	1078.63		8.85	✓
+50	1080.36		7.14	✓
13100	1082.07		5.43	✓
+50	1083.78		3.72	✓
14100	1085.49		2.01	✓
+50	1087.26	Reverse Error	0.24	✓

1075.48
93
1076.41
1.18
1075.23
12.27
1087.50
0.24
1087.26

T.P.

Whiskin
Snyder
Spoken

9/19/28

Sta	BS	H.I	FS
	902	1096.28	0.24 1087.26
15+00	1089.02		7.26 v
+50	1090.98		5.30 v
16+00	1092.54		3.74 v
+50	1094.30		1.98 v
	1168	1102.21	5.75 1090.53
17+00	1096.06		6.15 v
+50	1097.82		4.39 v
18+00	1099.58		2.63 3.13 v
+50	1101.34		0.87 1.87 v
	926	1109.60	
19+00	1103.10		6.50 7.00 v

T.P 1087.26
 9.02
 1096.28
 5.75
 1090.53
 11.68
 1102.21
 1.87
 1100.34
 9.26
 1109.60

T.P

F-0.5

F1.0 1100.34 T.P

F0.5

Sta		B.S.	H.I.	F.S.	
			1109.60		
+50	110478			4.82	✓
20+00	110642			3.18	✓
+50	110792			1.68	✓
21+00	110948	8.65	1117.63	0.12	0.62
B.M. #3		7.85	1117.61	7.85	1109.78
+50	1110.97			6.64	✓
22+00	1112.46			5.15	✓
+50	1113.95			3.66	4.16 ✓
23+00	1115.44			2.17	✓
+50	1116.92			0.69	1.69
				1.70	

1108.98	
8.65	
1117.63	1109.76
	7.85
	1117.61
	1.70
	1115.91
	11.00
	1126.91
	0.83
	1126.06
	10.36
	1136.42

Fo.5 1108.98
B.M. #3
1109.76

Fo.5

F1.0

1115.91 T.P

Sta	B.S.	H.I.	F.S.		
	11.00	1126.91			
24+00	1118.42		8.49	9.49	F.I.O
+50	1119.92		6.99	7.99	F.I.O
25+00	1121.40		5.51	6.01	F.O.5
+50	1122.98		3.93	4.43	F.O.5
26+00	1124.52		2.39	✓	
+50	1126.06		0.85	1126.06	T.P
	1036	1136.42			
27+00	1127.60		8.82	✓	
+50	1129.14		7.28	✓	
28+00	1130.64		5.78	✓	

Sta	BS	H.I	FS
		1136.42	
28+50	1132.18		4.24 ✓
29+00	1133.72		2.70 ✓
+50	1135.26	11.00	1.16 ✓ 1135.27
30+00	1136.80		9.45 ✓
+50	1138.35		7.90 ✓
31+00	1139.85		6.40 ✓
+50	1141.17		5.08 ✓
32+00	1142.59		3.83 ✓
+50	1143.72		2.53 ✓
			2.15 1144.10

1136.42
 1.17
 1135.25
 11.00
 1146.25

T.P

B.M. 4
 1144.05

B17⁰⁴

Sta	BS	H.I	FS	1144.05
	6.58	1150.63		

1144.05
6.58
<hr/> 1150.63

33700	1144.95		5.68	✓
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+50	1146.00		4.63	513
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Fo. 5

34700	1146.91		3.72	422
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Fo. 5

+50	1147.63		3.00	420
-----	---------	--	------	-----

F 1.0

35700	1148.18		2.45	✓
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6.58	1144.05
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BM 4

Finished 9/25/28 Revised Grade

Grade Sta.	B.S.	H.I.	F.S.	BM #
	392	1147.97		1144.05
34+00	1146.91		1.06	✓
+50	1146.00		1.97	2.47
33+00	1144.95		3.02	✓
+50	1143.72		4.25	✓
32+00	1142.59		5.38	✓
+50	1141.17		6.80	✓
31+00	1139.85		8.12	✓
+50	1138.35		9.62	1138.35
30+00	1136.80	0.18	1138.53	1.73
+50	1135.26		3.27	✓
29+00	1133.72		4.81	✓
+50	1132.18		6.35	✓
28+00	1130.64		7.89	✓
+50	1129.14		9.39	1129.14
27+00	1127.60	0.06	1129.20	1.60
+50	1126.06		3.14	✓
26+00	1124.52		4.68	✓

William Douglas-Cold,
Spohn
Snyder.

	1144.05
	392
	<hr/> 1147.97
	9.62
Fo.5	<hr/> 1138.35
	.18
	<hr/> 1138.53
	9.39
	<hr/> 1129.14
	0.06
	<hr/> 1129.20

T.P.

T.P.

Sta	B.S.	HT	FS	
			1129.20	
+50	1122.98		6.22	✓
25+00	1121.40		7.80	✓
+50	1119.92	336	1121.68	1.76 ✓
24+00	1118.42		3.26	✓
+50	1116.92		4.76	✓
23+00	1115.44		6.24	✓
+50	1113.95		7.73	✓
22+00	1112.46		9.22	✓
+50	1110.97	116	1112.13	10.71 ✓ 1110.97
21+00	1109.48	240	1112.16	2.68 ✓ 1109.73
+50	1107.92		4.24	✓
20+00	1106.42		5.74	✓
19+50	1104.78		7.38	✓
19+00	1103.10		9.06	✓
+50	1101.34		10.82	1132 ✓
18+00	1099.58	0.44	1101.28	1.70 ✓

1111.32	1109.76
1.56	2.40
1109.76	1112.16
	11.32
1118.32	1100.84
10.88	4.4
1118.32	1101.28
9.1	
1119.23	1110.97
10.65	
1108.58	1112.13
2.74	2.40
1111.32	1109.73

T.P.
B.M. #3 ✓
1109.76 F.O. 5

F.O. 5 1100.84

Sta

B-5

H1

FS

1101.28

+50 1097.82

3.46 ✓

17100 1096.06

5.22 ✓

+50 1094.30

6.98 ✓

16100 1092.54

8.74 ✓

+50 1090.98

10.30 ✓

15100 1089.02

12.26 ✓

+50 1087.26

14100 1085.49

+50 1083.78

Finished Grade

10/2/20

Hickey
Whistler
Snyder

Sta Grade HI F.S.

1152.25

34	1146.91		5.34	-	
+50	1147.63		4.62	-	6.2 F09
35	1148.18		4.07	-	5.3 F05
+50	1148.54		3.71	-	
36	1148.73		3.52	-	4.5 F03
+50	1148.73		3.52	-	
37	1148.55		3.70	-	4.7 F03
+50	1148.18		4.07	-	
38	1147.73	1150.10	2.37	-	
+50	1147.20		2.90	-	
39	1146.54		3.56	-	4.5 F03
+50	1145.73		4.37	-	
40	1144.81		5.29	-	6.2 F02
+50	1143.71		6.39	-	
41	1142.50		7.60	-	8.5 F02
+50	1141.13	1143.55	2.42	-	
42	1138.65		3.90	-	4.5 001
+50	1138.00		5.55	-	

BM#1 1144.05

8.20

1152.25

4.07

1148.18

1.92

1150.10

7.60

1142.50

1.05

1143.55

Sta	Grade	HI	FS	
		1143.55		
43	1136.22		7.33 - 81	F01
+50	1134.30		9.25 -	
44	1132.25		11.30 - 120	C00
+50	1130.12	1133.13	3.01 -	
45	1128.00		5.13 - 58	C00
+50	1125.85		7.28 -	
46	1123.75		9.38 -	C01
+50	1121.63		11.50 -	
47	1119.50	1122.39	2.89 - 3.5	C01
+50	1117.37		5.02 -	
48	1115.25		7.14 - 7.4	C04
+50	1113.12		9.27 -	C04
49	1111.00		11.39 -	
+50	1108.88	1111.77	2.89 -	
50	1106.75		5.02 -	C06
+50	1104.62		7.15 -	
51	1102.50		9.27 -	C01
+50	1100.37		11.40	

1143.55
 10.80
 1132.75
 0.38
 1133.13
 11.50
 1121.63
 0.76
 1122.39
 11.39
 1111.00
 0.77
 1111.77

Whiskin
Spahn
Snyder

10/3/28

BM 16

51a		B.S.	H.1	F.S.	1101.83
		0.25	1102.08		7.25
52	1098.19			3.89	✓
+50	1095.86			6.22	✓
53+00	1093.42			8.66	976 ✓
+50	1090.84		F0.5	11.24	1090.34 ✓
54+00	1088.14	1.75	1092.09	3.95	5.20 ✓
+50	1085.30		F0.5	6.79	✓
55+00	1082.40			9.69	10.60 ✓
+50	1079.50			12.59	1079.50 ✓
56+00	1076.60	0.90	1080.40	3.80	4.20 ✓
+50	1073.70			6.70	✓
57+00	1070.99			9.41	9.20 ✓
+50	1068.65			11.75	1068.65 ✓
58+00	1066.69	0.50	1069.15	2.46	2.85 ✓
+50	1065.11		E1.0	4.04	✓
59+00	1063.91			5.24	5.60 ✓
+50	1063.08			6.07	✓
60+00	1062.43			6.72	7.60 ✓

					1111.77
				9.93	9.94
				1101.84	134 1101.83
				1101.83	
				.25	
T.P.				1102.08	1080.38
				11.74	11.67
				1090.34	1068.71
				1.75	26.5
				1092.09	1071.36
				12.59	9.57
				1079.50	1061.79 ✓
				6.90	1.40
T.P.				1080.40	1063.19
				11.75	5.18
				1068.65	1058.01
				0.50	2.66
				1069.15	1060.67
					6.24
T.P.					11054.43

± Rod.

Sta	BS.	H.I.	FS.
		1069.15	
60+50	1061.79	Fo.5	7.36 1061.79
61+00	1061.15	191 1063.70	2.55 365
+50	1060.50	Fo.5	3.20
62+00	1059.86		3.84 5.00
+50	1059.22		4.48
63+00	1058.57		5.13 6.10
+50	1057.93		5.77 1057.93
+75	1057.47	Form L BS. 1057.48	357 1061.50 4.03
64+00 R	1057.15	1057.36	4.35
+25	1056.85	1057.26	4.65
+50	1056.58	1057.20	4.92
+75	1056.36	1057.17	5.14
65+00	1056.18	1056.99	5.32
+25			
+50			
+75			
66+00			

T.P.

1069.15
7.36
1061.79
1.91
1063.70
5.77
1057.93
3.57
1061.50
7.14
1054.36

T.P.

F.S.L ± Rod.

4.02
4.14
5.3
4.24
4.30
4.33
4.51
5.95

13.12

1054.36

Sta

Whiskin
Spohn
Snyder

10/6/28

B.S. H.1

F.S. Elex 105801

J.P.
Sta 63750

266

63775 R	105747	320	✓
63775 L	105748	319	✓
64100 R	105715	352	✓
64100 L	105736	331	✓
725 R	105685	382	✓
725 L	105726	341	✓
750 R	105658	409	✓
750 L	105720	347	✓
775 R	105636	431	✓
775 L	105717	350	✓
65100 R	105618	449	✓
700 L	105699	368	✓
725 R	105604	463	✓
725 L	105685	382	✓
750 R	105594	473	✓
750 L	105675	392	✓
775 R	105588	479	✓
775 L	105669	398	✓

F05

105801
266
106067

1060.67 1060.67
7.15 57.48
3.52 3.19
1060.67 1060.67
7.76 57.47
3.31 3.20

1060.67 1060.67
6.85 7.26
1060.67 3.82 53.41
5.88
4.79 1060.67 1060.67
6.58 7.20
1060.67 4.09 3.47
6.69 1060.67 1060.67
3.98 6.30 7.07
4.31 3.50
1060.67 1060.67
6.04 6.85
4.47 3.82
1060.67 1060.67
5.94 6.95
4.73 3.92

Sta	BS	H.I	F.S
		1060.67	
66+00 R	1055.86		481 ✓
L	1056.67		400 ✓
+25 R	1055.86		481 ✓
+25 L	1056.67	F0.5	400 ✓
+50 R	1055.86		481 ✓
+50 L	1056.67	F0.5	400 ✓
+75 R	1055.86		481 ✓
+75 L	1056.63	F0.5	404 ✓
67+00 R	1055.86		481 ✓
+00 L	1056.43	F0.5	424 ✓
+25 R	1055.86		481 ✓
+25 L	1056.22		445 ✓
+50 R	1055.86		481 ✓
+50 L	1056.07	F0.5	465 ✓

1060.67
6.24
 1054.43

1060.67 1060.67
5.86 6.67
 4.81 4.00
 1060.67 1060.67
5.86 6.63
 4.81 10 4.84

1060.67 1060.67
5.86 6.47
 4.81 4.24

1060.67 1060.67
6.22 6.02
 4.45 4.65

6.24 1054.43 1054.53

B.M

Sta	BS	H I	F.S.	T.P. sta 73+50 Elev. 1064.10
73+00	1063.20			
+50	1064.10	735	1071.45	
74+00	1065.00		6.45	✓
+50	1065.90		5.55	✓
75+00	1066.80		4.65	✓
+50	1067.70		3.75	✓
76+00	1068.60		2.85	✓
+50	1069.50		1.95	✓
77+00	1070.40		1.05	✓
+50	1071.30		0.15	1071.30 ✓
78+00	1072.20	Curve 8.07	1079.52	6.82 ✓
+50	1073.10		6.05	6.42 ✓
79+00	1074.00	± 6.1	6.10	5.52 ✓
+50	1074.90			4.62 ✓
				2.60 1076.92 ✓
		878	1085.70	0.63 1085.07 ✓

878

1064.10
 735
 1071.45
 8.07
 1079.52
 2.60
 1076.92
 8.78
 1085.70
 0.63
 1085.07

B.M. ^{chk.02}

T.P.

B.M. #9

T.P.

.02 ^{chk}

1085.05

Sta	Whiskin Spohn Snyder	Monday 10/8/28	Feqr	B.M. 7
	B.S.	H.1	FS	1054.43
67+75	1065.86	5.90	1062.33	4.47 ✓
68+00	1056.00			4.33 ✓
68+50	1056.11			4.22 ✓
69+00R	1056.41			3.92 ✓
69+00 L	1056.31		C-05	4.01 ✓
+25 R	1056.78			3.55 ✓
+25 L	1056.56			3.77 ✓
+50 R	1057.21			3.12 ✓
+50 L	1056.87			3.46 ✓
+75 R	1057.70		Fo.5	2.63 ✓
+75 L	1057.24			3.09 ✓
70+00 R	1058.15		Fo.5	2.18 ✓
70+00 L	1057.66			2.67 ✓
+25 R	1058.60		Fo.5	1.73 ✓
+25 L	1058.11			2.22 ✓
+50 R	1059.05		Fo.5	1.28 ✓
+50 L	1058.56			1.77 ✓
+75 R	1059.50		Fo.5	0.83 ✓
+75 L	1059.01	7.25	1066.23	7.22 ✓

1054.43
5.90
1060.33
1.25
1058.98
7.26
1066.23

136 1058.98 T.P.

1060.33
5.90
4.47

10/8/28

Sta	B.S	H.T	F.S	
		1066.23		
71+00 R	1059.95	F0.5	6.28	✓
71+00 L	1059.46	F0.5	6.77	✓
+25 R	1060.40	F1.0	5.83	✓
+25 L	1059.91	F1.0	6.32	✓
+50 R	1060.85	F1.0	5.38	✓
+50 L	1060.36	F0.5	5.87	✓
+75 R	1061.30	F1.0	4.93	✓
+75 L	1060.80	F0.5	5.43	✓
72+00 R	1061.63	F0.5	4.60	✓
72+00 L	1061.26		4.97	✓
+25 R	1061.96	F0.5	4.27	✓
+25 L	1061.71	F0.5	4.52	✓
+50 R	1062.28		3.95	✓
+50 L	1062.16	F0.5	4.07	✓
+75 R	1062.61		3.62	✓
+75 L	1062.61		3.62	✓
73+00	1063.20		3.03	✓
+50	1064.10		2.13	1064.10

1066.23
 2.13
 1064.10

T.P.

Sta	RS	H.1	FS	BM 17
	407	1196.32		1192.25
159+00	1189.76		6.56	
160+00	1191.56	Rail	4.76	
161+00	1192.65		3.67	
162+00	1193.03	4.00	1196.25	407 1192.25
			3.22	
163+00	1193.05	Rail	3.20	
164+00	1193.07		3.18	
165+00	1193.09		3.16	
166+00	1193.11	542	1196.11	556 1190.69
			3.00	
167+00	1192.90		3.21	

Whiskin Spolter Snyder. 10/23/28. Doody, Cold 73-3

$\frac{C.09}{25.2}$	$\frac{C.06}{24.2}$	$\frac{C.08}{24.5}$	$\frac{C.10}{25.5}$
$\frac{F0.3}{23.7}$	$\frac{F0.4}{22.7}$	$\frac{F0.8}{22.1}$	$\frac{F0.8}{23.1}$
$\frac{F1.1}{22.8}$	$\frac{F1.0}{21.8}$	$\frac{F1.8}{20.6}$	$\frac{F1.6}{21.6}$
$\frac{F0.2}{23.8}$	$\frac{F0.3}{22.8}$	$\frac{F1.4}{21.2}$	$\frac{F1.2}{22.2}$
$\frac{F0.7}{23.1}$	$\frac{F0.8}{22.1}$	$\frac{F1.9}{20.4}$	$\frac{F1.6}{21.4}$
$\frac{F1.8}{21.2}$	$\frac{F2.1}{20.2}$	$\frac{F2.2}{20.0}$	$\frac{F2.9}{21.0}$
$\frac{F2.4}{20.5}$	$\frac{F2.6}{19.5}$	$\frac{F1.8}{19.9}$	$\frac{F2.6}{20.9}$
$\frac{F1.4}{21.9}$	$\frac{F1.6}{20.9}$	$\frac{F1.8}{21.6}$	$\frac{F1.6}{21.6}$
$\frac{F0.5}{23.3}$	$\frac{F0.7}{22.3}$	$\frac{F1.5}{21.1}$	$\frac{F1.4}{22.1}$

BM 17 1192.25
Rail
TP

Sta

BS

H1

F3

1196.11

168700 119222

3.89

450

1196.93

368

1192.43

169700 119107

5.86

1705

170400 118955

7.38

$\frac{G09}{252}$

G06
242

F03
228

$\frac{F01}{238}$

T.P

$\frac{G10}{259}$

G11
249

G05
241

$\frac{G06}{251}$

$\frac{F08}{225}$

F12
215

F09
220

$\frac{F08}{230}$

Rock Sections 12/15/28

Richey
Parks
Spohn
Elev

574 BS HI FS

BM 172145 3.67 1184.81 1181.14

172+50

172+75

173+00

1176.58

BM 172+45 2.98 1184.12

1181.14

+25

+50

1171.95

0.81 1173.24 11.77

1172.36

+75

174

1167.33

+25

+50

1162.70

+75

11808
Right $\frac{4.6}{12.0} \frac{4.1}{6.0} \frac{4.0}{2.0} \frac{4.0}{7.0} \frac{4.1}{15.0} \frac{4.5}{20.0}$ Left
5.3 5.1 5.4 5.3 5.7 5.8
18.0 12.0 7.0 15.0 22.0

117801
 $\frac{5.6}{17.0} \frac{6.8}{6.0} \frac{7.3}{6.0} \frac{7.4}{10.0} \frac{8.5}{21.0}$

1174.72
 $\frac{7.3}{21.0} \frac{7.4}{14.0} \frac{9.4}{11.0} \frac{9.3}{20}$

1172.32
 $\frac{11.1}{17.0} \frac{11.8}{11.0} \frac{12.8}{11.0} \frac{12.5}{18.0}$

117006
 $\frac{3.9}{10.0} \frac{3.2}{7.0} \frac{4.4}{7.0} \frac{4.0}{15.0}$

116976
 $\frac{4.4}{9.0} \frac{4.5}{7.0} \frac{4.9}{17.0}$

116936
 $\frac{6.7}{15.0} \frac{5.9}{12.0}$

116596
 $\frac{8.1}{14.0} \frac{7.6}{9.0} \frac{7.3}{10.0} \frac{6.7}{10.0} \frac{7.2}{13.0}$

116336
 $\frac{10.3}{14.0} \frac{8.9}{10.0} \frac{9.9}{11.0} \frac{9.1}{11.0} \frac{9.9}{14.0}$

1173.26

572 55 HI 15 21ev

175

115208

0.48 1161.58 12.18 1161.08

+25

-150

115345

+75

176

114882

BM 176765 2.12 1153.20 1034 1151.22 1151.04

+25

+50

1144.19

BM 176765

+75

177

113957

0.47 1141.18 12.49 1140.71

Left ± Right

116156

$$\begin{array}{r} 12.5 \\ 15.0 \end{array}$$

$$\begin{array}{r} 11.7 \quad 11.9 \\ 10.0 \quad 15.0 \end{array}$$

$$\begin{array}{r} 1.0 \quad 1.4 \quad 1.3 \\ 13.0 \quad 9.0 \quad 5.0 \end{array}$$

$$\begin{array}{r} 116056 \\ 1.0 \\ \hline 2.8 \\ 14.0 \end{array}$$

No back

115756

$$\begin{array}{r} 3.9 \quad 3.7 \quad 4.0 \\ 13.0 \quad 11.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} 4.0 \quad 4.1 \quad 4.5 \quad 5.2 \quad 2.5 \\ \hline 9.0 \quad 13.0 \quad 18.0 \quad 21.0 \end{array}$$

115376

$$\begin{array}{r} 8.6 \quad 9.0 \\ 13.0 \quad 7.0 \end{array}$$

$$\begin{array}{r} 7.8 \quad 7.6 \quad 7.8 \quad 8.4 \\ \hline 10.0 \quad 17.0 \quad 21.0 \end{array}$$

115056

$$\begin{array}{r} 10.6 \quad 10.6 \quad 10.8 \\ 15.0 \quad 11.0 \quad 5.0 \end{array}$$

$$\begin{array}{r} 11.0 \quad 10.5 \quad 11.3 \\ \hline 13.0 \quad 23.0 \end{array}$$

114920

$$\begin{array}{r} 38 \quad 36 \quad 37 \quad 40 \\ 1.9 \quad 1.7 \quad 6 \quad 2 \end{array}$$

$$\begin{array}{r} 4.4 \quad 5.0 \quad 5.0 \\ \hline 9 \quad 22 \quad 27 \end{array}$$

114540

$$\begin{array}{r} 76 \\ 17 \end{array}$$

$$\begin{array}{r} 78 \quad 66 \quad 69 \quad 70 \\ \hline 12 \quad 20 \quad 27 \end{array}$$

114480

$$\begin{array}{r} 83 \\ 19 \end{array}$$

$$\begin{array}{r} 83 \quad 89 \quad 8.2 \quad 8.4 \quad 8.7 \quad 9.2 \quad 9.3 \\ 16 \quad 13 \quad 8 \quad 2 \quad 11 \quad 25 \quad 3.2 \end{array}$$

114310

$$\begin{array}{r} 11.7 \quad 10.7 \quad 10.2 \\ 16 \quad 12 \quad 7 \end{array}$$

$$\begin{array}{r} 10.1 \quad 11.1 \quad 12.0 \\ \hline 13 \quad 25 \end{array}$$

BS HI FS ELEV

114118

177+25

+50

6.29 1134.94

+75

178

10.87 1130.31

1.22 1129.96 12.44 1128.74

+17

+25

Slope 178+50

5.67 F13 F14

111383

Left

Right

2.6	25	24	37	2.3	26
13	8	8	9	22	28

113878

55	58	60	72
12	7	8	20

113244

69	68	77	8.5	26
23	17	11	8	17

113028

27	102	10.9	12.1
22	76	8	17

112806

13	14	17	19	35	30
20	12	3	8	12	20

112576

2.1	32	42	44	38
17	9	13	18	24

Reset slope 2/6/29
 sta BS HI FS Elev
 BM #20 12.47 112630 111383
 +50 0.62 112568
 10.64 1136.81 0.13 1126.17
 176 6.50 113031
 12.21 114752 1.50 113531
 +50 12.58 115474
 177 7.95 113957
 9.24 1154.70 2.06 114546
 3.60 1151.10 115108

MK
 FT
 ch

FR.0
 235

223

196

F05
 20.6

C50
 33.8

32.8

290

250

C57
 25.3

24.3

C59
 25.4

24.4

5/10/29

Richey
Griswold
Rand
Ashcraft

B.M. #9

213 1087.18

1085.05

201 1083.09 6.10 1081.08

80

7.29 1075.80

81

5.49 1077.60

82

3.69 1079.90

83

1.89 1081.20

8.46 1091.37 0.18 1082.91

84

8.26 1083.11

85

6.13 1085.24

B.M. #9

6.36 1091.41 6.36 1085.01 1085.05

86

3.92 1087.49

87

1.66 1089.75

T.P. Hub to
10th Rd

0.31 1091.10

88

1092.00

 $\frac{C 0.7}{25.5}$ $\frac{C 3.3}{28.8}$ $\frac{C 0.5}{24.6}$ $\frac{C 2.6}{28.2}$ $\frac{F 0.5}{23.3}$ $\frac{C 1.3}{26.1}$ $\frac{F 2.2}{21.2}$ $\frac{C 0.2}{24.6}$ $\frac{F 3.2}{21.1}$ $\frac{F 0.7}{22.7}$ $\frac{F 3.6}{22.5}$ $\frac{F 2.9}{21.0}$ $\frac{F 3.0}{21.5}$ $\frac{F 3.0}{21.5}$ $\frac{F 1.7}{21.6}$ $\frac{C 0.1}{23.7}$

222

24.4

5/16/29 Richey Ashcraft
Rand
Griswold

BM 145100 1.18 1170.99 1169.31

145 3.36 1167.13

144 2.99 1167.50

143 2.61 1167.88

142 2.25 1168.24

141 7.85 1173.60 4.74 1165.75

140 4.78 1168.82

139 4.86 1168.74

138 7.17 1166.43

137 1.40 1168.92 6.08 1167.52

136 5.45 1163.47

135 8.32 1160.60

134 1.97 1160.68 10.21 1158.71

F3.4
22.9

F0.1
23.5

F2.9
21.1

F1.7
21.3

F2.6
20.7

F2.1
20.7

F2.5
20.5

F1.2
21.9

F0.7
23.1

F0.2
23.7

East sideroad
25.0

C1.0
26.2

C1.1
26.8

C3.6
29.8

C0.7
24.9

C1.4
27.9

F1.9
20.2

C0.4
23.6

1160.68

136

2.85 1157.83

135

5.16 1155.52

BM#15 8.96 1162.81 6.76 1153.92 1153.85

134

7.56 1155.25

133

5.89 1156.92

132

2.47 1160.34

5.59 1166.93 1.47 1161.34

131

3.89 1163.04

130

3.10 1163.83

129

3.26 1163.67

BM#14

2.85 1164.75 1164.79

128

3.43 1163.50

3.21 1167.60 2.54 1164.39

127

4.26 1163.34

BM#14 2.85 1167.64 2.85 1164.75 1164.79

 $\frac{F3.1}{223}$ $\frac{F1.5}{20.6}$ $\frac{F2.8}{21.7}$ $\frac{F3.5}{23.5}$ $\frac{F1.8}{20.9}$ $\frac{F1.6}{21.6}$ $\frac{C0.8}{25.0}$ $\frac{C2.9}{29.5}$ $\frac{C1.0}{25.8}$ $\frac{C0.7}{24.7}$ $\frac{C0.2}{24.6}$ $\frac{C1.2}{25.9}$ $\frac{F1.1}{22.7}$ $\frac{C0.2}{24.6}$ $\frac{F0.1}{24.7}$ $\frac{C1.5}{26.2}$ $\frac{C0.9}{25.5}$ $\frac{C2.2}{27.8}$ $\frac{C0.4}{24.8}$ $\frac{C2.0}{27.2}$

116764

126			4.47	116217	
125			4.64	1163.00	
124			4.64	1163.00	
	7.16	1167.25	7.55	1160.09	
123			4.25	1163.00	
122			4.25	1163.00	
BM #13	3.47	1167.33	3.47	1163.78	116386
121			3.97	1163.36	
120			2.90	1164.43	
	6.32	1171.03	2.62	1164.71	
119			5.20	1165.83	
118			3.77	1167.26	
117			2.34	1168.69	

$$\frac{F0.5}{23.4}$$

$$\frac{C1.0}{25.7}$$

$$\frac{F1.6}{21.6}$$

$$\frac{F0.2}{24.0}$$

$$\frac{F2.9}{20.9}$$

$$\frac{F1.5}{21.8}$$

$$\frac{F2.7}{19.7}$$

$$\frac{F2.6}{20.7}$$

$$\frac{F2.1}{21.3}$$

$$\frac{F1.4}{22.7}$$

$$\frac{F1.8}{21.7}$$

$$\frac{F0.6}{23.2}$$

$$\frac{F1.5}{21.7}$$

$$\frac{F0.6}{23.4}$$

$$\frac{F1.4}{21.8}$$

$$\frac{F0.7}{23.1}$$

$$\frac{F0.9}{22.4}$$

$$\frac{C0.6}{25.4}$$

$$\frac{C0.0}{24.1}$$

$$\frac{C0.8}{25.2}$$

117103

116 1.00 1170.03

4.49 1173.91 1.61 1169.42

113 3.56 1170.35

114 4.87 1169.04

BM# 12 4.15 1169.76 1169.75

113 1166.86

112 1163.05

111 1158.25

110 1153.34

109 1148.43

108 1143.52

107 1138.61

$\frac{F0.6}{22.7}$

$\frac{F0.9}{22.7}$

$\frac{F0.5}{23.1}$

$\frac{F1.5}{21.6}$

$\frac{C0.8}{25.0}$

$\frac{F0.7}{23.3}$

$\overline{25.9}$

$\overline{27.0}$

$\overline{26.4}$

$\overline{26.8}$

$\overline{26.2}$

$\overline{26.7}$

$\overline{27.1}$

$\overline{27.9}$

6/5/29

M. Pichey
P. Pichey
C. Rand.
G. Griswold

Rock sections

1168.18

112 + 25

112

5.13 1163.05

+ 75

+ 50

7.97 1160.71

+ 25

8.90 1159.48

111

9.23 1158.25

+ 75

+ 50

1155.80

6305

210

303

68.18

Subgrade

19 ±
6.5

C05

no rock except boulder 20 yd

15 ±
8.2

C05

+ 35 C03 bare rock

C02

F01

5/21/24
 M Richey
 F. Richey
 C Rand
 T/Viser

6.28 1060.84 1059.56
 188+50 7.50 1057.24
 189 5.48 1055.36
 3.14 1063.65 0.30 1060.54
 189+50 6.38 1057.27
 190 4.91 1058.74
 190+50 3.79 1059.86
 191 2.65 1061.00

$\frac{C 0.4}{22.3}$	$\overline{21.7}$	$\overline{29.6}$	$\frac{F 4.6}{30.6}$
$\frac{C 3.4}{18.5}$	$\overline{17.5}$	—	—
$\frac{C 2.6}{16.6}$	$\overline{15.6}$	$\overline{25.0}$	$\frac{C 2.3}{26.0}$
$\frac{C 0.7}{17.1}$	$\overline{16.1}$	$\overline{22.5}$	$\frac{C 1.5}{22.5}$
$\frac{F 1.1}{20.2}$	$\overline{19.2}$	$\overline{19.5}$	$\frac{F 0.4}{20.5}$
$\frac{F 1.9}{20.0}$	$\overline{19.0}$	$\overline{21.0}$	$\frac{F 1.5}{22.0}$

5/22/22

N. Richey
F. Richey
E. Richey
T. Richey

Reset slopes to new backslope

BM 176+65 1276 1163.84 1151.08

175+00 1158.08

175+50 10.09 1153.45

176+00 15.02 1148.82

3.54 1154.77 12.61 1151.23

176+50 10.58 1144.19

177+00 5.89 15.20 1139.57

2.93 1145.46 12.24 1142.53

177+50 10.52 1134.94

2.70 1135.88 12.28 1133.18

178+00 5.57 1130.31

178+50 1125.68

0.31 1124.28 11.91 1123.77

BM 179+10 10.52 1113.76 1112.83

1267

C0.1

$\frac{C7.1}{36.0}$

$\frac{C7.2}{33.3}$

F0.2

C0.2

$\frac{C5.9}{33.9}$

$\frac{C2.4}{26.1}$

F1.4

C0.2

$\frac{C5.4}{33.6}$

$\frac{C2.8}{26.3}$

F1.0

C0.5

$\frac{C5.5}{33.4}$

$\frac{C2.1}{24.7}$

C0.0

F0.5

$\frac{C5.5}{33.3}$

$\frac{F1.5}{20.7}$

F1.4

F0.4

$\frac{C4.4}{33.2}$

$\frac{F0.1}{24.0}$

F1.3

F0.2

F1.0

5/27/29

Richey
Rand
Kiser

BM#9 10.82 1095.87 10850.5

88 3.87 1092.00

9.07 1103.84 110 1094.77

89 9.60 1094.24

90 7.36 1096.98

10.19 1109.10 4.93 1098.91

91 10.38 1098.72

92 8.14 1100.96

93 5.90 1102.20

94 3.66 1105.44

8.85 1113.91 4.04 1105.06

95 6.23 1107.68

BM#10 1110.27

96 3.99 1109.92

$$\frac{F1.1}{22.2}$$
$$\frac{C0.4}{24.4}$$
$$\frac{C0.0}{24.3}$$
$$\frac{C4.0}{30.0}$$
$$\frac{C0.7}{25.2}$$
$$\frac{C2.9}{28.8}$$
27.2
$$\frac{C1.8}{29.3}$$
 offset 2'
$$\frac{C4.0}{31.2}$$
$$\frac{C2.1}{27.6}$$
$$\frac{C4.9}{32.8}$$
$$\frac{C0.8}{25.6}$$
$$\frac{C4.3}{30.6}$$
$$\frac{F7.4}{30.5}$$
$$\frac{F5.4}{27.5}$$
$$\frac{F4.9}{25.3}$$
$$\frac{F5.9}{28.3}$$
$$\frac{F2.7}{20.7}$$
$$\frac{C0.9}{25.6}$$

	1113.91				
	12.73	1126.05	0.59	1113.32	
97			13.89	112.16	
98			11.73	1114.32	
99			7.47	1116.58	
	1.82	1119.00	8.87	1117.18	
BM #10	8.74	1119.01	8.74	1110.26	1110.27
	5.37	1122.56	1.82	1117.19	
100			4.74	1118.82	
101			2.50	1120.06	
	11.50	1133.23	0.83	1121.73	
102			9.91	1123.32	
BM #11	3.71	1129.71	7.19	1126.04	1126.00
103			4.12	1125.59	
104			1.84	1127.87	
	10.35	1139.20	0.86	1128.85	
105			8.90	1130.30	

C12
26.1

C40
27.8

C05
26.4

C6.8
34.2

C0.6
25.0

C6.5
33.6

F7.5
35.9

F0.1
23.1

F2.7
22.5

F1.3
23.1

C1.7
26.4

C5.8
32.4

F2.2
23.1

F2.2
31.6

F1.5
21.3

F3.1
20.5

F0.1
23.7

F0.1
22.4

1139.20

106

5.33 1133.87

10.48 1148.93

0.75 1138.45

107

18.32 1138.61

108

5.41 1143.52

11.04 1159.87

0.10 1148.83

109

11.44 1148.43

110

6.53 1153.24

111

1.62 1158.25

12.74 1172.54

0.27 1159.60

112

9.49 1163.05

113

5.68 1166.86

114

1169.04

BM #12

2.79 1169.75 1169.75

$\frac{F1.3}{22.4}$

$\frac{F1.3}{21.2}$

$\frac{C4.9}{31.3}$

$\frac{C1.6}{26.5}$

$\frac{C4.3}{31.3}$

$\frac{C4.2}{31.2}$

$\frac{C3.1}{28.8}$

$\frac{C1.8}{26.8}$

$\frac{C1.8}{27.1}$

$\frac{C0.5}{24.9}$

$\frac{C1.6}{26.2}$

$\frac{C1.5}{26.1}$

$\frac{C1.7}{26.7}$

$\frac{C2.1}{26.8}$

$\frac{C1.9}{25.9}$

$\frac{C0.0}{24.0}$

6/5/29

M. P. Riency
F. R. Riency
G. Griswold
C. Rand

Work Stakes

BM #21	7.66	1062.22			1054.56
Bridge floor S end			10.26	1051.96	
187+50 R			9.99	1052.23	-
L			10.50	1051.72	-
187+00 R			8.52	1053.70	F 1.0
L			9.73	1052.49	-
186+50 R			6.55	1055.67	-
L			7.94	1054.28	F 0.5
186+00 R			3.76	1058.46	-
L			5.15	1057.07	C 0.5
185+50 R			-0.07	1062.27	-
L	13.02	1073.90	1.34	1060.88	-
185+00 R			7.06	1066.84	F 0.5
L			8.45	1065.45	-
184+50 R			2.44	1071.46	F 0.5
L			3.83	1070.07	-
	13.10	1085.20	1.80	1072.10	
BM 184+00			3.16	1082.04	1081.96
184+00 R			9.56	1075.64	
L			10.50	1074.70	

6/5/29

M. P. Cheney
F. P. Cheney
C. Rand
G. Griswold

Work stakes

BM #21	2.50	1057.06		1054.56
Bridge floor Nend		5.27	1051.79	
188+00 R		5.11	1051.95	C 0.5
L		4.88	1052.18	
188+50 R		3.86	1053.20	C 1.0
L		2.62	1054.34	C 0.5
189+00 R		1.84	1055.22	C 1.0
L	5.09	1062.10	0.04 0.05	1057.02 1057.01
189+50 R		4.97	1057.13	C 1.0
L		3.17	1058.23	F 1.0
190+00 R		3.50	1058.60	C 0.5
L		2.15	1059.95	F 1.0
190+50 R		2.38	1059.72	F 0.5
L		1.93	1060.17	F 1.0
191+00 R				
L				

6/5/29

Rock Sections

BM # 11 643	1132.43	1126.00
104 +50	3.43	1129.00
+75		
105	2.13	1130.30
+25		
+50	0.51	1131.92
11.14 14335	0.22	1132.21
106	9.48	1033.87
+50	7.19	1136.16
+75		
107	4.75	1138.61
+25	3.51	1139.84
+50	2.28	1141.07
+75	1.05	1142.30
9.40 1152.00	0.75	1142.60
108	8.48	1143.52
109	3.57	1148.43

Spows

subgrade

C05E

19	$\frac{19}{2.6}$	18
5.9		4.6

19	$\frac{19}{3.6}$	19
5.1		3.6

OK

19	$\frac{19}{3.7}$	19
3.2		4.0

19		
3.2		

no at 20-E

OK

19	$\frac{19}{2.9}$	
3.2		

meat 18-E

OK

F02

19	$\frac{19}{10.2}$	$\frac{19}{1.6}$
10.2		1.6

19	$\frac{19}{8.1}$	$\frac{19}{1.1}$
8.1		1.1

F07

12	$\frac{12}{6.8}$	$\frac{19}{6.6}$
6.8		6.6

F08

12	$\frac{12}{5.9}$	$\frac{19}{5.8}$
5.9		5.8

F05

19	$\frac{19}{4.0}$	
4.0		

F05

19	$\frac{19}{2.8}$	$\frac{19}{4.0}$
2.8		4.0

Bogot +60

F09

19	$\frac{19}{10.8}$	$\frac{19}{11.4}$
10.8		11.4

Check	Levels	From	To	Elev
BS	HI	FS		1192.25
383	1196.08			
		427	1191.81	TP
554	1197.35			
		1145	1185.90	TP
160	1187.50			
		636	1181.14	BM
208	1183.22			
		1139	1171.83	TP
073	1172.56			
		1160	1160.96	TP
124	1162.20			
		1112	1151.08	BM
373	1154.81			
		1222	1142.59	TP
078	1143.47			
		1231	1131.16	TP
006	1131.22			
		1180	1119.42	TP
009	1119.51	569	1113.82	BM

Whisker & Notes.
Snyder red
Snyder chain Rod.

BM Spike in 18 Maple Sta 172+45
100' Rt of E Elev 1181.14

New BM #19
BM Spike in 6 Cherry. Located Sta 176+65
100' Lt of E Elev 1151.08
1151.08

BM #20 Spike in twin Ash 50 E of E. 179+10
Elev 1113.83

B.M. 20

B.S.

4.1
1119.31

FS

Flex

1113.82

13.01

1106.50

T.P.

0.50

1107.00

13.56

1093.94

0.65

1094.59

New
B.M.

12.63

1081.96

0.84

1082.80

10.27

1072.53

T.P.

0.71

1073.24

10.53

1062.71

T.P.

0.63

1063.34

B.M. #21

8.85

1054.49

1054.56

1066.84
71
1067.55

New B.M. Spike in 20" Apple Sta. 184+00

Located 100 ft Lt. of ~~E~~ Elev 1081.96

5/31/29

W. Richy
F. Ricketts
S. Merritt
Barton

Reset slopes new grade

BM # 21 4.51 1052.07 1054.56

187+50 7.21 1051.86

187+00 6.44 1052.63

186+50 4.65 1054.42 OK.

186+00 1.86 1057.21 F20

185+50 - 1.95 1061.02

13.05 1067.61 4.51 1054.56

185+00 2.02 1065.59

13.15 1080.40 0.36 1067.25

184+50 10.19 1070.21

BM 154+00	10.20	1087.80	2.80	1077.60	
	5.79	1087.76	5.79	1082.81	1081.96
184+00			15.92	1074.84	

183+50 8.30 1079.46 C03

10.72 1095.37 3.11 1084.65

$\frac{F5.1}{33.7}$	$\frac{F4.7}{32.7}$	$\frac{F4.7}{25.4}$	$\frac{F4.6}{26.4}$
---------------------	---------------------	---------------------	---------------------

$\frac{F4.5}{31.8}$	$\frac{F5.4}{30.8}$	$\frac{F4.5}{27.6}$
---------------------	---------------------	---------------------

$\frac{F6.9}{33.6}$	$\frac{F6.3}{32.6}$	$\frac{F5.6}{27.2}$	$\frac{F4.9}{28.2}$
---------------------	---------------------	---------------------	---------------------

$\frac{F9.4}{41.0}$	—	$\frac{F6.8}{29.6}$	$\frac{F6.8}{30.6}$
---------------------	---	---------------------	---------------------

$\frac{F4.0}{25.0}$	$\frac{F3.0}{24.0}$	$\frac{F8.7}{37.5}$
---------------------	---------------------	---------------------

$\frac{C6.8}{35.7}$	—	$\frac{19.8}{20.8}$
---------------------	---	---------------------

$\frac{C7.4}{37.8}$	—
---------------------	---

$\frac{C9.0}{35.1}$	$\frac{C8.5}{34.1}$
---------------------	---------------------

$\frac{C5.2}{31.4}$	$\frac{30.4}{30.4}$
---------------------	---------------------

1085.37

183+00

11.29 1089.08

182+50

6.67 1088.70

13.14 1104.81 3.70 1091.67

182+00

11.48 1093.33

181+50

6.86 1097.95

181+00

2.24 1102.57

180+50

1107.19

180+00

1111.82

$\frac{C4.7}{31.2}$

$\frac{C3.5}{29.3}$

$\frac{C3.4}{28.3}$

$\frac{F1.7}{22.1}$

$\frac{F1.7}{26.5}$

$\frac{F4.0}{25.0}$

19.0

$\frac{F2.4}{20.0}$

BM 176+65 12.15 1163.23

1157.08

175+25A 7.33 1155.90 -

L 7.61 1155.62 -

175+50A 5.16 1158.07 -

L 5.29 1157.94 -

Set 174+75

174+75A 1160.25

L 1160.29

174+50A 0.67 1162.56 Sub
10.2

L 0.40 1162.83 -

174+25A 1169.87

L 1165.37

174+50A 1167.17

L 1167.83

1.6
67

120440
120
1203.20

10.7
9.2
05.8

61 1199.48 60
2.41
1201.89 49

1053.09 1071.40
9.17 64.44
1062.26 69.6

108825
13.06
1101.31 6.13
1071.40 1.3
62.04 56
1122.25 283
1196.08

1211.18 1071.40
4.57 65.57 1071.40
5.87 67.32

1215.75
5.21

1201.81
9.62

1210.54
5.23

1211.43
1.98

1205.77

1209.45
0.23

1163.23 3.19

1153.74 1212.58

249 2.43

5.52 1215.01

7.37

1207.62

1215.70 1064.14
4.57 1061.40

1211.13 3.74

1101.28 1102.21
1099.58 94.30
01.70 7.91

1061.40 1061.40
1062.50 11
1060.20 10.07
10.07 1072.57

1119.51 1118.25
3.83 7.82
5.68

1070.2 6.17
6.17 1066.40
6.17 61.40

1110.42
97.610

6.6

64.14 5.00

TABLE IX.—CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.12	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w = 16.2 and h = 5.3, cu. yds. = 1.48 + .028 + .089 = 1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) = h, and $\frac{1}{2}$ the roadbed = w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR

CROSS SECTIONING

PLEASE RETURN TO
Roadway 16 feet wide Side Slopes 1 on 1 1/2.

For single track Embankment

GEAUGA COUNTY ENGINEER

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	II
0	8.0	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	9.0	9.4
1	9.5	9.7	9.8	9.9	10.0	10.1	10.2	10.3	10.4	10.5	10.9
2	11.0	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	12.0	12.4
3	12.5	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	13.5	13.9
4	14.0	14.2	14.3	14.4	14.5	14.6	14.8	14.9	15.0	15.1	15.4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	17.3
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	18.8
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	20.3
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	21.8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	23.3
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	24.8
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	26.3
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	27.8
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	29.3
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	30.8
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	32.3
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	33.8
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	35.3
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	36.8
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	38.3
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	39.8
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	41.3
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	42.8
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	44.3
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	45.8
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	47.3
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	48.8
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	50.3
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	51.8
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	53.3
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	54.8
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	56.3
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	57.8
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	59.3
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	60.8
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	62.3
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	63.8
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	65.3
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	66.8
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	68.3
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	69.8

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

